

25-07445

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22

LM7705 Low-Noise Negative Bias Generator

Technical [Documents](http://www.ti.com/product/LM7705?dcmp=dsproject&hqs=td&#doctype2)

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-
-
- Turnon Time 500 µs
-
-

-
-
- Low-Voltage Split-Power Supplies

1 Features 3 Description

Tools & **[Software](http://www.ti.com/product/LM7705?dcmp=dsproject&hqs=sw&#desKit)**

¹ The LM7705 device is a switched capacitor voltage • Regulated Output Voltage −0.232 V inverter with a low noise, −0.23 V fixed negative Output Voltage Tolerance 5% voltage regulator. This device is designed to be used

Output Voltage Ripple 4 mV_{PP} voltage regulator. This device is designed to be used

with low voltage amplifiers to enable the amplifiers with low voltage amplifiers to enable the amplifiers • Maximum Output Current 26 mA output to swing to zero volts. The −0.23 V is used to Supply Voltage 3 V to 5.25 V
maintaining less then 5.5 V across the amplifier. Rail-
for Rail-output amplifiers cannot output zero volts to-Rail output amplifiers cannot output zero volts • Quiescent Current 78 µA when operating from a single-supply voltage and can Shutdown Current 20 nA **Fig. 20 is a set of the set of the set of the Shutdown Current 20 nA** set of the set of saturation voltage being amplified by following gain stages. A small negative supply voltage will prevent • Operating Temperature Range −40°C to 125°C the amplifiers output from saturating at zero volts and 8-Pin VSSOP Package **• 1998** • 1999 • Will help maintain an accurate zero through a signal processing chain. Additionally, when an amplifier is used to drive an input of the ADC, the amplifier can **2 Applications** output a zero voltage signal and the full input range Frue Zero Amplifier Outputs **Example 20** of an ADC can be used. The LM7705 device has a • Portable Instrumentation shutdown pin to minimize standby power

Device Information[\(1\)](#page-0-0)

(1) For all available packages, see the orderable addendum at the end of the data sheet.

Typical Application

Table of Contents

4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision B (March 2013) to Revision C Page

• Added *Pin Configuration and Functions* section, *ESD Ratings* table, *Feature Description* section, *Device Functional Modes*, *Application and Implementation* section, *Power Supply Recommendations* section, *Layout* section, *Device and Documentation Support* section, and *Mechanical, Packaging, and Orderable Information* section [1](#page-0-3)

Changes from Revision A (November 2008) to Revision B Page

• Changed layout of National Data Sheet to TI format [19](#page-18-3)

STRUMENTS

XAS

5 Pin Configuration and Functions

Pin Functions

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) Typical values represent the most likely parametric norm as determined at the time of characterization. Actual typical values may vary over time and will also depend on the application and configuration. The typical values are not tested and are not ensured on shipped production material.

6.2 ESD Ratings

(1) Human Body Model, applicable std. MIL-STD-883, Method 3015.7.

(2) Field induced Charge-Device Model, applicable std. JESD22–C101–C. (ESD FICDM std of JEDEC).

(3) Machine model, applicable std JESD22–A115–A (ESSD MM srd of JEDEC).

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6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

6.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953.](http://www.ti.com/lit/pdf/spra953)

6.5 3.3-V Electrical Characteristics

Unless otherwise specified, all limits are ensured for $T_A = 25^{\circ}$ C, V_{DD} = 3.3 V, V_{SS} = 0 V, SD = 0 V, C_{FLY}= 5 µF, C_{RES} = 22 µF, $C_{OUT} = 22 \mu F$.

(1) All limits are specified by testing or statistical analysis.

(2) Typical values represent the most likely parametric norm as determined at the time of characterization. Actual typical values may vary over time and will also depend on the application and configuration. The typical values are not tested and are not specified on shipped production material.

3.3-V Electrical Characteristics (continued)

Unless otherwise specified, all limits are ensured for $T_A = 25^{\circ}$ C, V_{DD} = 3.3 V, V_{SS} = 0 V, SD = 0 V, C_{FLY}= 5 µF, C_{RES} = 22 µF, $C_{\text{OUT}} = 22 \mu F$.

6.6 5-V Electrical Characteristics

Unless otherwise specified, all limits are ensured for $T_A = 25^{\circ}$ C, $V_{DD} = 5.0$ V, $V_{SS} = 0$ V, SD = 0V, C_{FLY} = 5 µF, C_{RES} = 22 µF, $C_{OUT} = 22 \mu F$.

(1) All limits are specified by testing or statistical analysis.

(2) Typical values represent the most likely parametric norm as determined at the time of characterization. Actual typical values may vary over time and will also depend on the application and configuration. The typical values are not tested and are not specified on shipped production material.

EXAS **RUMENTS**

6.7 Typical Characteristics

Typical Characteristics (continued)

Typical Characteristics (continued)

Typical Characteristics (continued)

7 Detailed Description

7.1 Overview

The LM7705 is a switched capacitor voltage inverter with a low-noise, −0.23-V fixed negative bias output. The part will operate over a supply voltage range of 3 V to 5.25 V. Applying a logical low level to the SD input will activate the part, and generate a fixed −0.23-V output voltage. The part can be disabled; the output is switched to ground level, by applying a logical high level to the SD input of the part.

7.2 Functional Block Diagram

7.3 Feature Description

7.3.1 Supply Voltage

The LM7705 will operate over a supply voltage range of 3 V to 5.25 V, and meet the specifications given in the *3.3-V Electrical [Characteristics](#page-3-2)* Table. Supply voltage lower than 3.3 V will decrease performance (The output voltage will shift towards zero, and the current sink capabilities will decrease) A voltage higher than 5.25 V will exceed the *Absolute [Maximum](#page-2-2) Ratings* ratings and therefore damage the part.

7.3.2 Output Voltage and Line Regulation

The fixed and regulated output voltage of −0.23 V has tight limits, as indicated in the *3.3-V [Electrical](#page-3-2) [Characteristics](#page-3-2)* table, to ensure a stable voltage level. The usage of the pre- and post regulator in combination with the charge pump inverter ensures good line regulation of 0.29%/V

7.3.3 Output Current and Load Regulation

The LM7705 can sink currents more than 26 mA, causing an output voltage shift to −200 mV. A specified loadregulation of 0.14% mA/V ensures a minor voltage deviation for load current up to 20 mA.

7.3.4 Quiescent Current

The LM7705 consumes a quiescent current less than 100 µA. Sinking a load current, will result in a current conversion efficiency better than 90%, even for load currents of 1 mA, increasing to 98% for a current of 5mA.

7.4 Device Functional Modes

7.4.1 General Amplifier Application

This section will discuss a general DC coupled amplifier application. First, one of the limitations of a DC coupled amplifier is discussed. This is illustrated with two application examples. A solution is a given for solving this limitation by using the LM7705.

Due to the architecture of the output stage of general amplifiers, the output transistors will saturate. As a result, the output of a general purpose op amp can only swing to a few 100 mV of the supply rails. Amplifiers using CMOS technology do have a lower output saturation voltage. This is illustrated in [Figure](#page-10-0) 22. For example, Texas Instruments' LM7332 can swing to 200 mV to the negative rail, for a 10-kΩ load, over all temperatures.

Device Functional Modes (continued)

INPUT VOLTAGE (V)

Figure 22. Limitation of the Output of an Amplifier

The introduction of operational amplifiers with output rail-to-rail drive capabilities is a strong improvement and the (output) performance of op amps is for many applications no longer a limiting factor. For example, Texas Instruments' LMP7701 (a typical rail-to-rail op amp), has an output drive capability of only 50 mV over all temperatures for a 10-kΩ load resistance. This is close to the lower supply voltage rail.

However, for true zero output applications with a single supply, the saturation voltage of the output stage is still a limiting factor. This limitation has a negative impact on the functionality of true zero output applications. This is illustrated in [Figure](#page-10-1) 23.

Figure 23. Output Limitation for Single-Supply True Zero Output Application

In the *One-Stage, [Single-Supply](#page-10-2) True Zero Amplifier* section, two applications will be discussed, showing the limitations of the output stage of an op amp in a single supply configuration:

- A single stage true zero amplifier, with a 12-bit ADC back end.
- A dual stage true zero amplifier, with a 12-bit ADC back end.

7.4.1.1 One-Stage, Single-Supply True Zero Amplifier

This application shows a sensor with a DC output signal, amplified by a single supply op amp. The output voltage of the op amp is converted to the digital domain using an Analog to Digital Converter (ADC). [Figure](#page-10-3) 24 shows the basic set-up of this application.

Figure 24. Sensor With DC Output and a Single-Supply Op Amp

Device Functional Modes (continued)

The sensor has a DC output signal that is amplified by the op amp. For an optimal signal-to-noise ratio, the output voltage swing of the op amp must be matched to the input voltage range of the Analog to Digital Converter (ADC). For the high side of the range this can be done by adjusting the gain of the op amp. However, the low side of the range cannot be adjusted and is affected by the output swing of the op amp.

Example:

Assume the output voltage range of the sensor is 0 to 90 mV. The available op amp is a LMP7701, using a 0/+5- V supply voltage, having an output drive of 50 mV from both rails. This results in an output range of 50 mV to 4.95V.

Select two resistors values for R_{G1} and R_{F1} that result in a gain of 50x. The output of the LMP7701 must swing from 0 mV to 4.5 V. The higher value is no problem, however the lower swing is limited by the output of the LM7701 and won't go below 50 mV instead of the desired 0 V, causing a non-linearity in the sensor reading. When using a 12-bit ADC, and a reference voltage of 5 V (having an ADC step size of approximate 1.2 mV), the output saturation results in a loss of the lower 40 quantization levels of the ADCs dynamic range.

7.4.1.2 Two-Stage, Single-Supply True Zero Amplifier

This sensor application produces a DC signal, amplified by a two cascaded op amps, having a single supply. The output voltage of the second op amp is converted to the digital domain. [Figure](#page-11-0) 25 shows the basic setup of this application.

Figure 25. Sensor With DC Output and a 2-Stage, Single-Supply Op Amp

The sensor generates a DC output signal. In this case, a DC coupled, 2-stage amplifier is used. The output voltage swing of the second op amp must me matched to the input voltage range of the Analog to Digital Converter (ADC). For the high side of the range this can be done by adjusting the gain of the op amp. However, the low side of the range can't be adjusted and is affected by the output drive of the op amp.

Example:

Assume; the output voltage range of the sensor is 0 to 90 mV. The available op amp is a LMP7702 (Dual LMP7701 op amp) that can be used for A_1 and A_2 . The op amp is using a 0/+5-V supply voltage, having an output drive of 50 mV from both rails. This results in an output range of 50 mV to 4.95 V for each individual amplifier.

Select two resistors values for ${\sf R}_{\sf G1}$ and ${\sf R}_{\sf F1}$ that result in a gain of 10x for the first stage (A₁) and a gain of 5x for the second stage (A₂) The output of the A₂ in the LMP7702 must swing from 0V to 4.5 V. This swing is limited by the 2 different factors:

- 1. The high voltage swing is no problem; however the low voltage swing is limited by the output saturation voltage of A_2 from the LM7702 and will not go below 50 mV instead of the desired 0 V.
- 2. Another effect has more impact. The output saturation voltage of the first stage will cause an offset for the input of the second stage. This offset of A_1 is amplified by the gain of the second stage (10x in this example), resulting in an output offset voltage of 500mV. This is significantly more that the 50 mV (V_{DSAT}) of A₂.

When using a 12-bit ADC, and a reference voltage of 5 Volt (having an ADC step size of approximate 1.2 mV), the output saturation results in a loss of the lower 400 quantization levels of the ADCs dynamic range. This will cause a major non-linearity in the sensor reading.

Device Functional Modes (continued)

7.4.1.3 Dual-Supply, True Zero Amplifiers

The limitations of the output stage of the op amp, as indicated in both examples, can be omitted by using a dual supply op amp. The output stage of the used op amp can then still swing from 50 mV of the supply rails. However, the functional output range of the op amp is now from ground level to a value near the positive supply rail. [Figure](#page-12-0) 26 shows the output drive of an amplifier in a true zero output voltage application.

Figure 26. Amplifier Output Drive With a Dual-Supply

Disadvantages of this solution are:

- The usage of a dual-supply instead of a simple single supply is more expensive.
- A dual supply voltage for the op amps requires parts that can handle a larger operating range for the supply voltage. If the op amps used in the current solution cannot handle this, a redesign can be required.

A better solution is to use the LM7705. This low-noise negative bias generator has some major advantages with respect to a dual-supply solution:

- Operates with only a single positive supply, and is therefore a much cheaper solution.
- The LM7705 generates a negative supply voltage of only −0.23 V. This is more than enough to create a Truezero output for most op amps.
- In many applications, this *small* extension of the supply voltage range can be within the abs max rating for many op amps, so an expensive redesign is not necessary.

In the *Typical [Application](#page-15-0)* section, a typical amplifier application will be evaluated. The performance of an amplifier will be measured in a single supply configuration. The results will be compared with an amplifier using a LM7705 supplying a negative voltage to the bias pin.

EXAS **ISTRUMENTS**

8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

8.1.1 Functional Description

The LM7705, low-noise negative bias generator, can be used for many applications requiring a fixed negative voltage. A key application for the LM7705 is an amplifier with a true zero output voltage using the original parts, while not exceeding the maximum supply voltage ratings of the amplifier.

The voltage inversion in the LM7705 is achieved using a switched capacitor technique with two external capacitors (C_{FLY} and C_{RES}). An internal oscillator and a switching network transfers charge between the two storage capacitors. This switched capacitor technique is given in [Figure](#page-13-2) 27.

Figure 27. Voltage Inverter

The internal oscillator generates two anti-phase clock signals. Clock 1 controls switches S1 and S2. Clock 2 controls switches S3 and S4. When Switches S1 and S2 are closed, capacitor C_{FLY} is charged to V⁺. When switches S3 and S4 are closed (S1 and S2 are open) charge from C_{FLY} is transferred to C_{RES} and the output voltage OUT is equal to $-V^*$.

Due to the switched capacitor technique, a small ripple will be present at the output voltage with a frequency of the oscillator. The magnitude of this ripple will increase for increasing output currents. The magnitude of the ripple can be influenced by changing the values of the used capacitors.

8.1.2 Technical Description

As indicated in *Functional [Description](#page-13-3)*, the main function of the LM7705 is to supply a stabilized negative bias voltage to a load, using only a positive supply voltage. A general block diagram for this charge pump inverter is given in [Figure](#page-13-4) 28. The external power supply and load are added in this diagram as well.

Figure 28. LM7705 Architecture

The architecture given in [Figure](#page-13-4) 28 shows that the LM7705 contains 3 functional blocks:

- Pre-regulator
- Charge pump inverter
- Post-regulator

Application Information (continued)

The output voltage is stabilized by:

- Controlling the power supplied from the power supply to the charge pump input by the pre-regulator
- The power supplied from the charge pump output to the load by the post-regulator.

A more detailed block diagram of the negative bias generator is given in [Figure](#page-14-0) 29. The control of the preregulator is based on measuring the output voltage of the charge pump. The goal of the post-regulator is to provide an accurate controlled negative voltage at the output, and acts as a lowpass filter to attenuate the output voltage ripple. The voltage ripple is a result of the switching behavior of the charge pump and is dependent of the output current and the values of the used capacitors.

Figure 29. Charge Pump Inverter With Input and Output Control

In *[Charge](#page-14-1) Pump Theory*, a simple equation will be derived that shows the relation between the ripple of the output current, the frequency of the internal clock generator and the value of the capacitor placed at the output of the LM7705.

8.1.3 Charge Pump Theory

This section uses a simplified but realistic equivalent circuit that represents the basic function of the charge pump. The schematic is given in [Figure](#page-14-2) 30.

Figure 30. Charge Pump

When the switch is in position A, capacitor ${\sf C}_{\sf FLY}$ will charge to voltage ${\sf V}_1.$ The total charge on capacitor ${\sf C}_{\sf FLY}$ is Q_1 = C_{FLY} x V ₁. The switch then moves to position B, discharging C_{FLY} to voltage V₂. After this discharge, the charge on ${\sf C}_{\sf FLY}$ will be ${\sf Q}_2$ = ${\sf C}_{\sf FLY}$ \times ${\sf V}_2.$ The charge has been transferred from the source ${\sf V}_1$ to the output ${\sf V}_2.$ The amount of charge transferred is:

$$
\Delta q = q1 - q2 = C_{FLY} (V1 - V2)
$$
\nIn the switch changes between A and B at a frequency f, the charge transfer per unit time, or current is:

\n
$$
I = f \Delta q = f C_{FLY} (V1 - V2)
$$

When the switch changes between A and B at a frequency f, the charge transfer per unit time, or current is:

$$
I = f \Delta q = f C_{FLY} (V1 - V2)
$$

The switched capacitor network can be replaced by an equivalent resistor, as indicated in [Figure](#page-15-1) 31.

(2)

(3)

Application Information (continued)

Figure 31. Switched Capacitor Equivalent Circuit

The value of this resistor is dependent on both the capacitor value and the switching frequency as given in [Equation](#page-15-2) 3

$$
I = \frac{V1 - V2}{\left(\frac{1}{f C_{FLY}}\right)} = \frac{V1 - V2}{R_{EQ}}
$$

The value for R_{EQ} can be calculated from [Equation](#page-15-3) 3 and is given in Equation 4

$$
R_{\text{EQ}} = \left(\frac{1}{f C_{\text{FLY}}}\right) \tag{4}
$$

[Equation](#page-15-3) 4 show that the value for the resistance at an increased internal switching frequency, allows a lower value for the used capacitor.

8.2 Typical Application

This section shows the measurement results of a true zero output amplifier application with an analog to digital converter (ADC) used as back-end. The biasing of the op amp can be done in two ways:

- A single supply configuration
- A single supply in combination with the LM7705, extending the negative supply from ground level to a fixed –0.23 Voltage.

Figure 32. Typical True Zero Output Voltage Application With or Without LM7705

Typical Application (continued)

8.2.1 Design Requirements

The key specifications of the used components are shown in [Table](#page-16-0) 1.

8.2.2 Detailed Design Procedure

8.2.2.1 Basic Setup

The basic setup of this true zero output amplifier is given in [Figure](#page-15-4) 32. The LMP7701 op amp is configured as a voltage follower to demonstrate the output limitation, due to the saturation of the output stage. The negative power supply pin of the op amp can be connected to ground level or to the output of the negative bias generator, to demonstrate the V_{DSAT} effect at the output voltage range.

The output voltage of the LMP7701 is converted to the digital domain using an ADC122S021. This is an 12-bit analog to digital converter with a serial data output. Data processing and graphical displaying is done with a computer. The negative power supply pin of the op amp can be connected to ground level or to the output of the negative bias generator, to demonstrate the effect at the output voltage range of the op amp.

8.2.3 Application Curves

The output voltage range of the LMP7701 has been measured, especially the range to ground level. A small DC signal, with a voltage swing of 50 mV_{PP} is applied to the input. The digitized output voltage of the op amp is measured over a given time period, when its negative supply pin is connected to ground level or connected to the output of the LM7705.

[Figure](#page-17-1) 33 shows the digitized output voltage of the op amp when its negative supply pin is connected to ground level. The output of the amplifier saturates at a level of 14 mv (this is in line with the typical value of 18 mV given in the datasheet) The graph shows some fluctuations (1-bit quantization error). [Figure](#page-17-1) 34 show the digitized output voltage of the op amp when its negative supply pin is connected to the output of the LM7705. Again, the graph shows some 1-bit quantization errors caused by the voltage ripple and output noise. In this case the op amps output level can reach the true zero output level.

[Figure](#page-17-1) 33 and [Figure](#page-17-1) 34 show that:

- With a single supply, the output of the amplifier is limited by the V_{DSAT} of the output stage.
- The amplifier can be used as a true zero output using a LM7705.
- The quantization error of the digitized output voltage is caused by the noise and the voltage ripple.
- Using the LM7705 does not increase the quantization error in this set up.

9 Power Supply Recommendations

To prevent large variations at the V_{DD} pin of the package it is recommended to add a decouple capacitor as close to the pin as possible.

10 Layout

10.1 Layout Guidelines

The LM7705 is a switched capacitor voltage inverter. This means that charge is transferred from different external capacitors, to generate a negative voltage. For this reason the part is very sensitive for contact resistance between the package and external capacitors. TI also recommends to use low ESR capacitors for C_{FLY} , C_{RES} and C_{OUT} in combination with short traces.

The output voltage noise can be suppressed using a small RF capacitor, will a value of, for example, 100 nF.

10.2 Layout Examples

[Figure](#page-18-4) 35 contains a layout example for the LM7705.

Figure 35. Example PCB Layout: Top layer

11 Device and Documentation Support

11.1 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms](http://www.ti.com/corp/docs/legal/termsofuse.shtml) of [Use.](http://www.ti.com/corp/docs/legal/termsofuse.shtml)

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11.2 Trademarks

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11.3 Electrostatic Discharge Caution

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

11.4 Glossary

[SLYZ022](http://www.ti.com/lit/pdf/SLYZ022) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check<http://www.ti.com/productcontent>for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

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Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE MATERIALS INFORMATION

Texas
Instruments

TAPE AND REEL INFORMATION

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

TEXAS
INSTRUMENTS

PACKAGE MATERIALS INFORMATION

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*All dimensions are nominal

DGK (S-PDSO-G8)

PLASTIC SMALL-OUTLINE PACKAGE

NOTES: A. All linear dimensions are in millimeters.

This drawing is subject to change without notice. **B.**

Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per end.

- Body width does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
- E. Falls within JEDEC MO-187 variation AA, except interlead flash.

DGK (S-PDSO-G8)

PLASTIC SMALL OUTLINE PACKAGE

NOTES: Α. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. Publication IPC-7351 is recommended for alternate designs.
- D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
- E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

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